

A decorative background featuring a network of thin grey lines connecting various colored nodes (blue, green, yellow, and orange) of different sizes. The nodes are scattered across the white background, with some clusters and many isolated points. The overall design is modern and scientific.

*The National Academies of*  
SCIENCES • ENGINEERING • MEDICINE

# ILLUSTRATING THE IMPACT OF THE MATHEMATICAL SCIENCES

# The Illustrating Mathematics Project

*A collection of narratives and graphics will be the central focus of a consensus report that broadly describes the fundamental role of the mathematical sciences in the U.S. economy, national security, health and medicine, and other science, engineering, and technology domains. Visit <https://www.nationalacademies.org/our-work/illustrating-the-impact-of-the-mathematical-sciences> for more information.*

This webinar series is presented by  
**the Board on Mathematical Sciences and Analytics**

and is made possible with support from

**the National Science Foundation Division of Mathematical Sciences**



# ILLUSTRATING MATHEMATICS

## 2020 Webinar Series, 3-4pm ET

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# ILLUSTRATING MATHEMATICS

## Supercompatibility and the Design of Materials



**Richard James,  
University of Minnesota**



© NYU Photo Bureau: Kahn  
**Robert Kohn,  
New York University**



**Irene Fonseca,  
Carnegie Mellon University  
(moderator)**

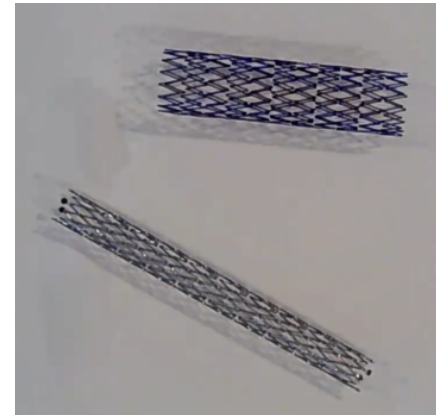
# Supercompatibility and the design of materials

Richard James  
University of Minnesota  
[james@umn.edu](mailto:james@umn.edu)

Robert Kohn  
Courant Institute of Mathematical Sciences  
[kohn@cims.nyu.edu](mailto:kohn@cims.nyu.edu)

# The reversibility of phase transformations

Click [here](#) to watch a demonstration of Nickel-Titanium Stents.

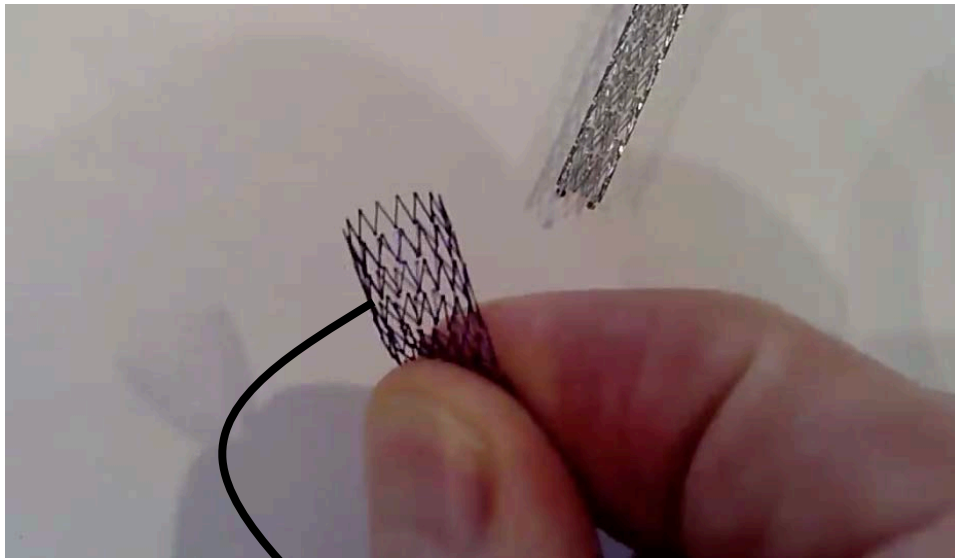


Click [here](#) to watch demonstration of  $-15^{\circ}\text{C}$  Tin phase transformation.

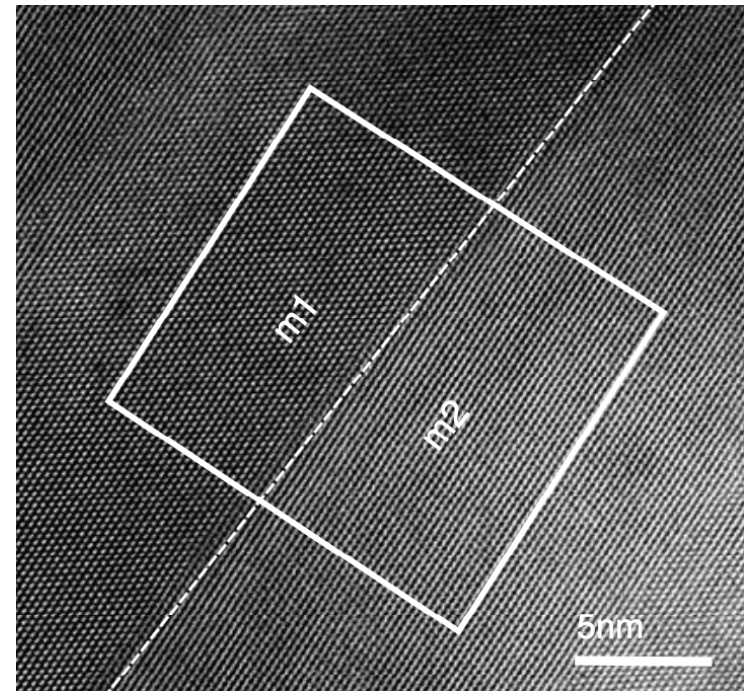




# Back to NiTi



x 5000



x 50

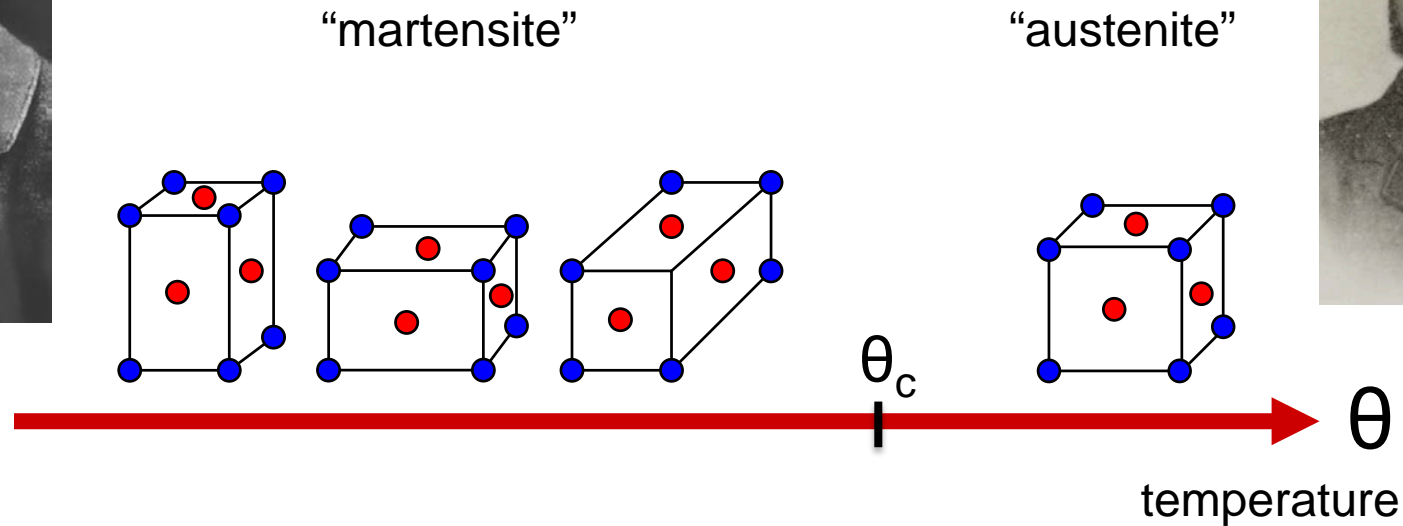
Adolph Karl  
Gottfried Martens



Sir William Chandler  
Roberts-Austin



# Phase transformations

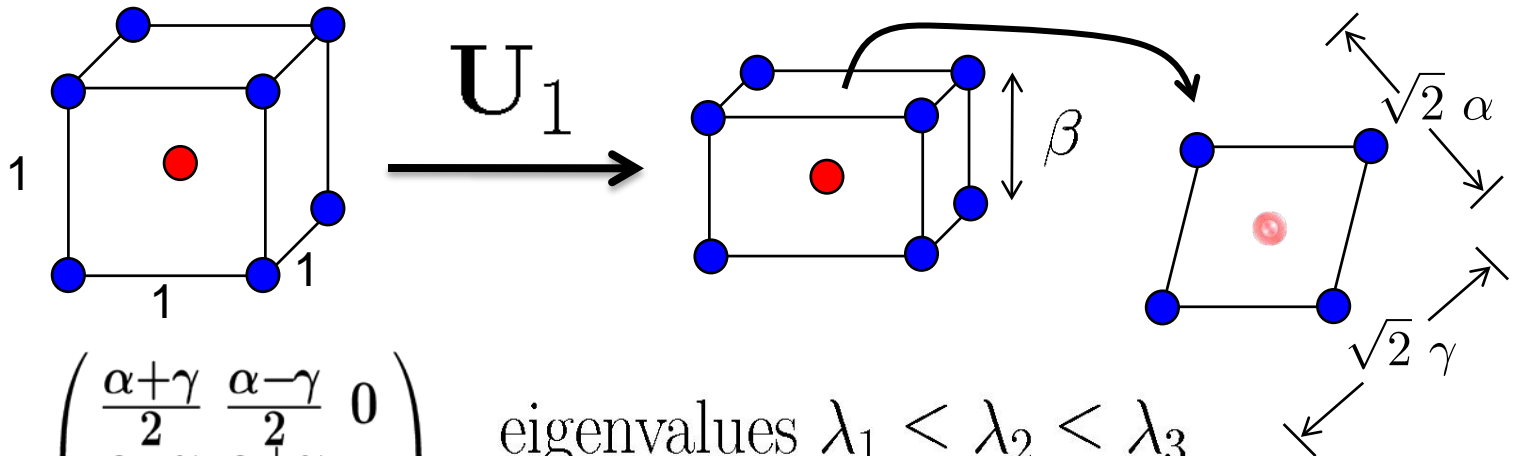


➔ more precisely, change of crystal structure, no diffusion:  
**martensitic phase transformations**



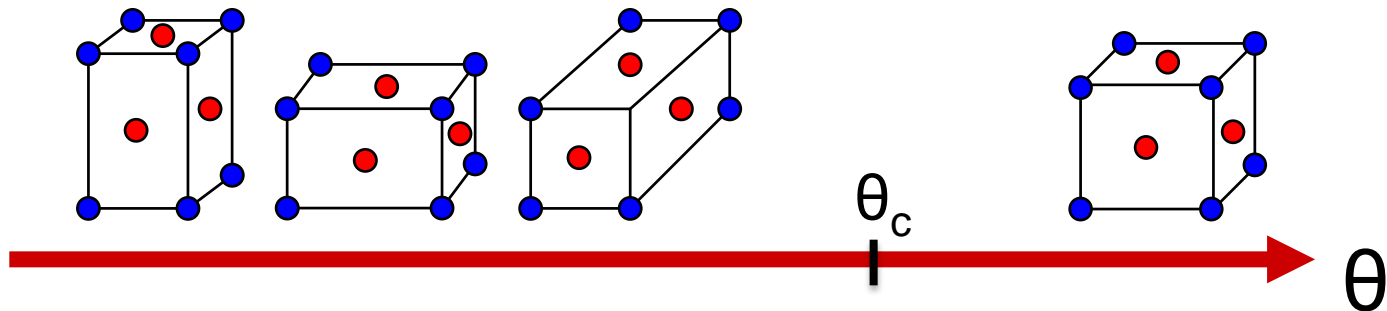
# Transformation matrix

(Transformation stretch matrix)

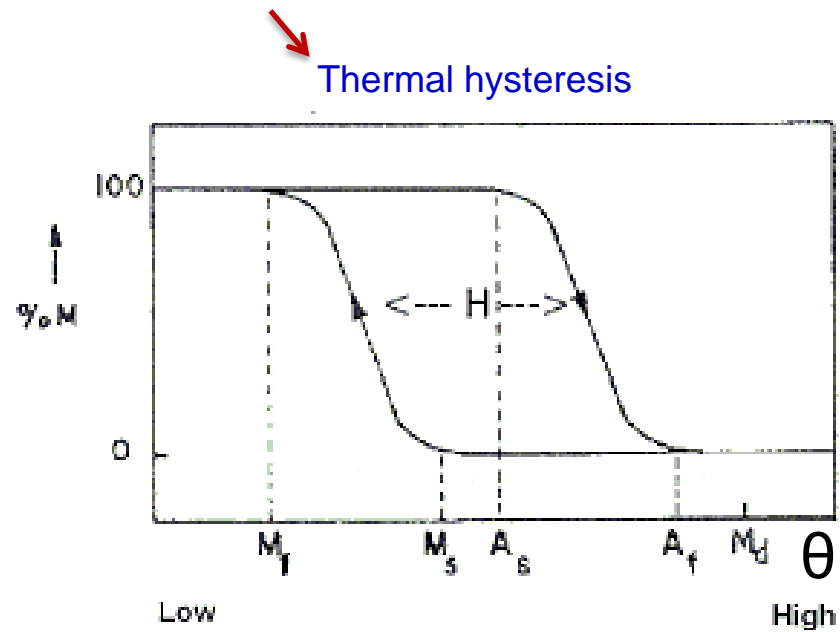
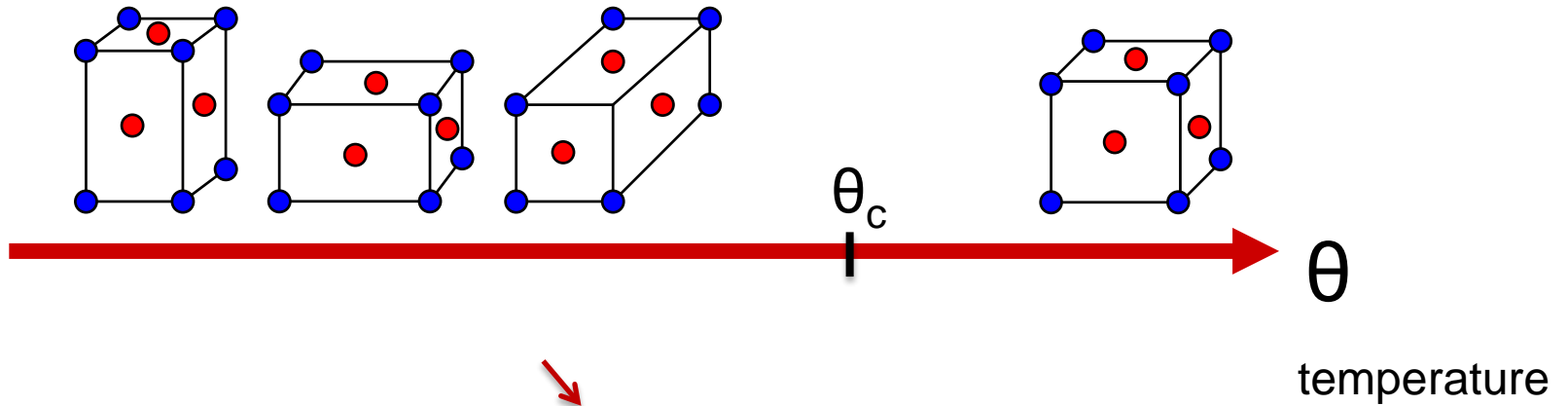


$$\mathbf{U}_1 = \begin{pmatrix} \frac{\alpha+\gamma}{2} & \frac{\alpha-\gamma}{2} & 0 \\ \frac{\alpha-\gamma}{2} & \frac{\alpha+\gamma}{2} & 0 \\ 0 & 0 & \beta \end{pmatrix}$$

eigenvalues  $\lambda_1 \leq \lambda_2 \leq \lambda_3$

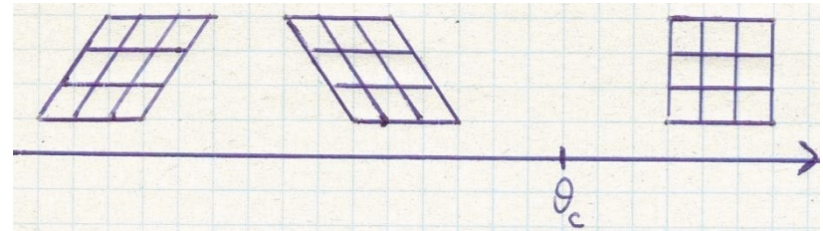
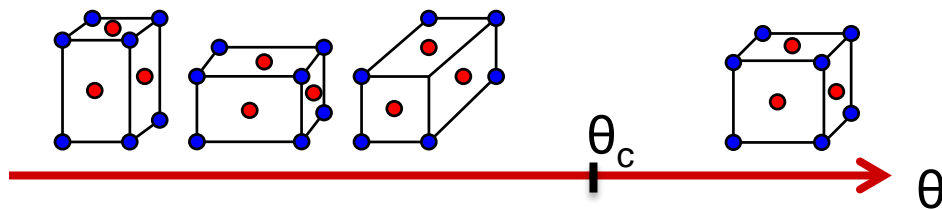


# Hysteresis loops



# Essential mechanisms

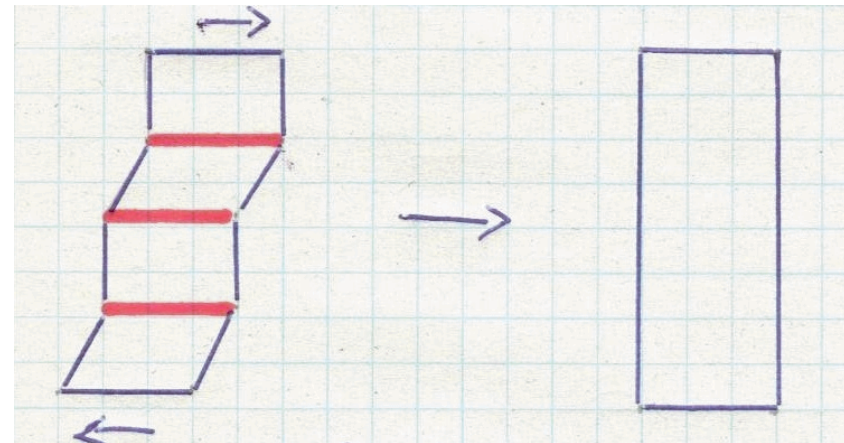
Microscopic mechanisms of **superelasticity** and **shape-memory** involve a symmetry-breaking phase transformation



- at temp  $\theta > \theta_c$  there is a single preferred lattice structure
- $\theta < \theta_c$  there are several (symmetry-related) preferred structures

## Superelastic behavior ( $\theta > \theta_c$ )

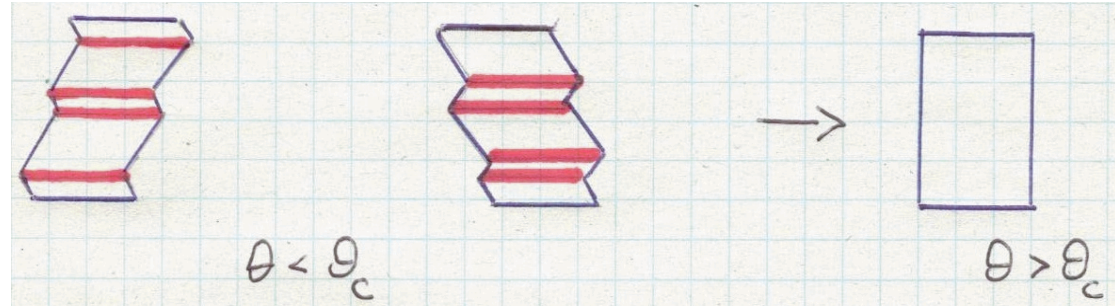
- loading nucleates martensite & moves phase boundaries
- unloading  $\Rightarrow$  return to austensite



# Essential mechanisms

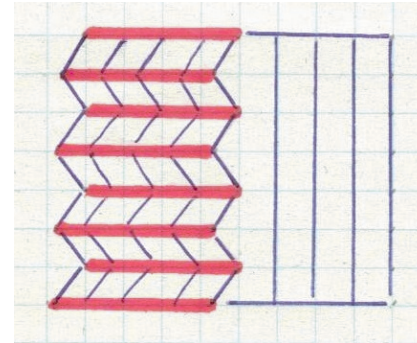
## Shape-memory behavior ( $\theta < \theta_c$ )

- deformation (without stress) by mixing martensite variants
- heating restores lattice to austenite



## Microstructure

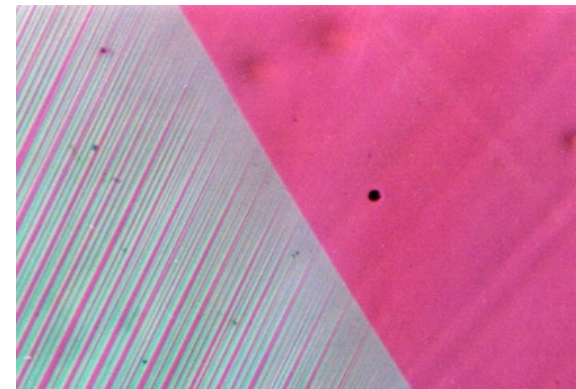
- permits mixture of martensite variants to mimic austenite
- but: transition layer isn't stress-free



$$\theta = \theta_c$$

## Warning: 2D schematic oversimplifies

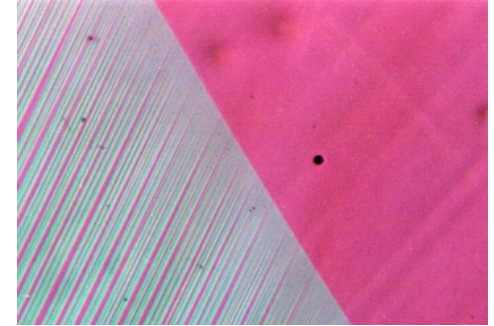
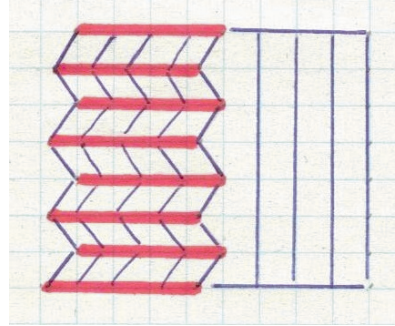
- in reality there are many variants of martensite
- microstructure predominates, except in special circumstances



# Mathematical description

Use the framework of **nonlinear elasticity**: let  $\mathbf{x} \mapsto \mathbf{y}(\mathbf{x})$  take austenite (high symmetry) lattice to actual configuration

- $\mathbf{y}(\mathbf{x})$  is continuous but only piecewise smooth
- preferred values of  $\nabla \mathbf{y}$  are set by the phase transformation



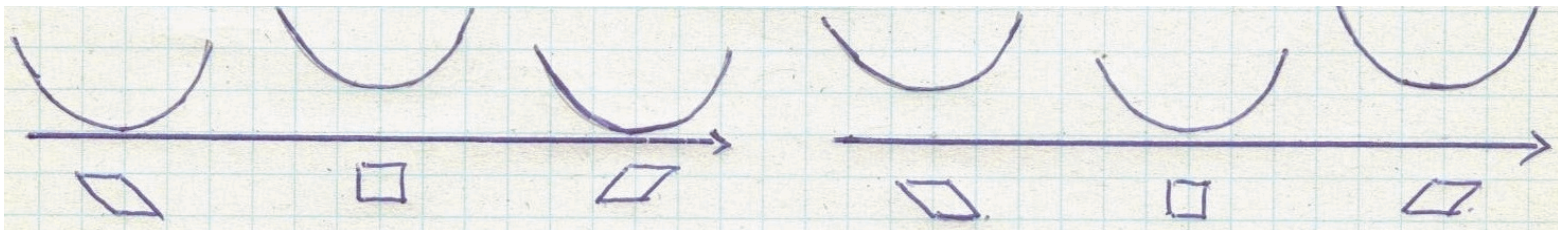
Predicting structure is a problem in the **calculus of variations**:

$$\min_{\text{bdry conds}} \int_{\text{ref domain}} \varphi(\nabla \mathbf{y}(\mathbf{x}), \theta) d\mathbf{x} + \text{energy of the loading device}$$

where  $\varphi$  is a multiwell energy density, with local minima at the preferred structures:

$$\varphi(\nabla \mathbf{y}, \theta), \quad \theta < \theta_c$$

$$\varphi(\nabla \mathbf{y}, \theta), \quad \theta > \theta_c$$





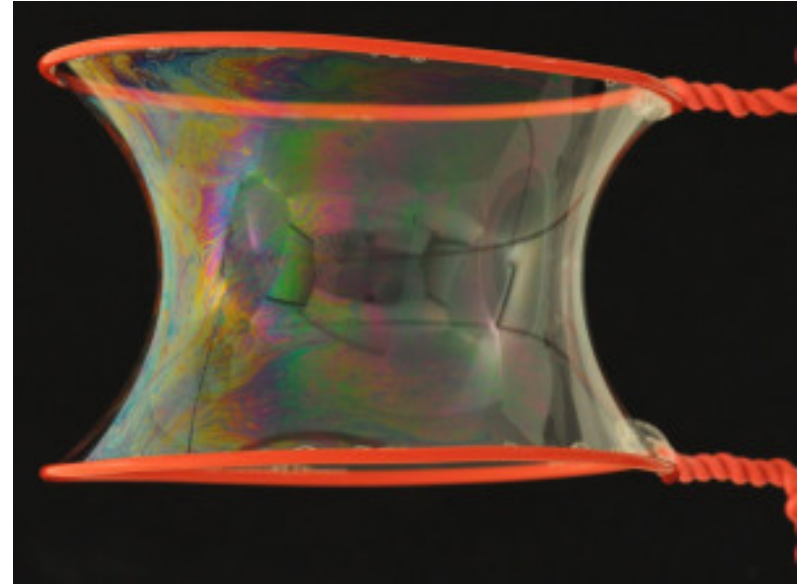
# A different kind of variational problem

In many familiar examples a solution exists. Goals for analysis include

- finding it numerically
- understanding its singularities

Ours is different: a solution may not exist, if microstructure is needed. Goals include

- understanding when microstructure is needed
- learning how interfacial energy sets the character and scale of phase mixtures



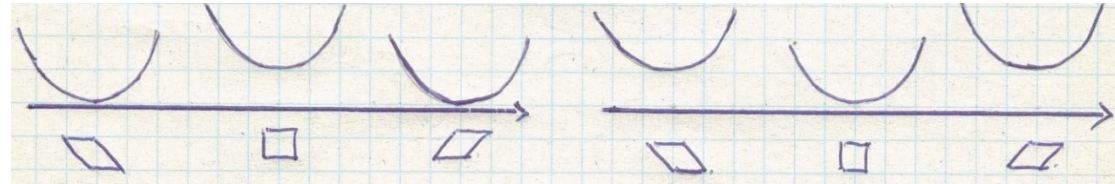
[mathematicalgarden.wordpress.com](http://mathematicalgarden.wordpress.com)



# Free energy and energy wells

$$\varphi(\nabla \mathbf{y}, \theta), \theta < \theta_c$$

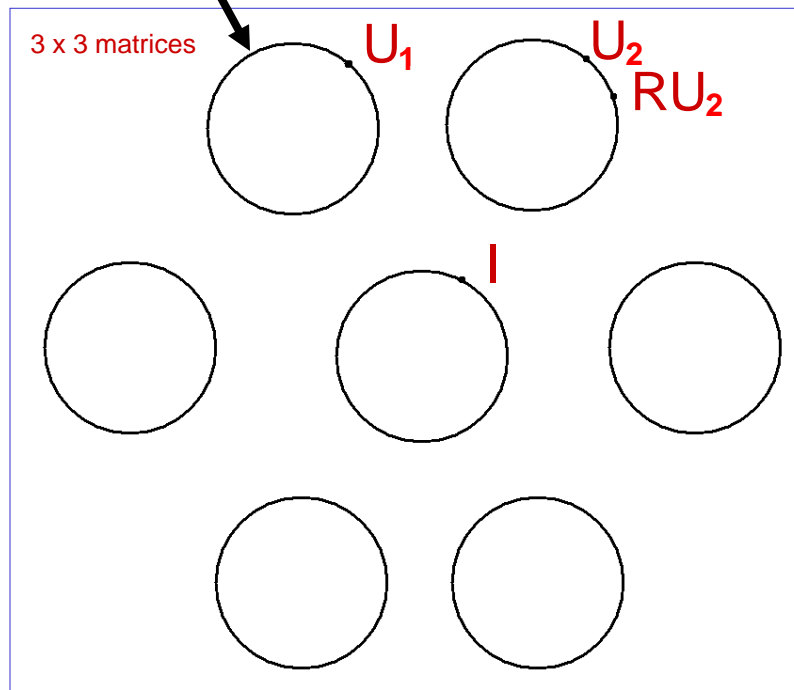
$$\varphi(\nabla \mathbf{y}, \theta), \theta > \theta_c$$



$$\min_{BC} \int_{\Omega} \varphi(\nabla \mathbf{y}(\mathbf{x}), \theta) d\mathbf{x}$$

$\theta = \theta_c$

minimizers...



$$\mathbf{U}_1 = \begin{pmatrix} \frac{\alpha+\gamma}{2} & \frac{\alpha-\gamma}{2} & 0 \\ \frac{\alpha-\gamma}{2} & \frac{\alpha+\gamma}{2} & 0 \\ 0 & 0 & \beta \end{pmatrix}$$

$$\mathbf{U}_2 = \begin{pmatrix} \frac{\alpha+\gamma}{2} & \frac{\gamma-\alpha}{2} & 0 \\ \frac{\gamma-\alpha}{2} & \frac{\alpha+\gamma}{2} & 0 \\ 0 & 0 & \beta \end{pmatrix}$$

$$\mathbf{U}_3 = \begin{pmatrix} \frac{\alpha+\gamma}{2} & 0 & \frac{\alpha-\gamma}{2} \\ 0 & \beta & 0 \\ \frac{\alpha-\gamma}{2} & 0 & \frac{\alpha+\gamma}{2} \end{pmatrix}$$

$$\mathbf{U}_4 = \begin{pmatrix} \frac{\alpha+\gamma}{2} & 0 & \frac{\gamma-\alpha}{2} \\ 0 & \beta & 0 \\ \frac{\gamma-\alpha}{2} & 0 & \frac{\alpha+\gamma}{2} \end{pmatrix}$$

$$\mathbf{U}_5 = \begin{pmatrix} \beta & 0 & 0 \\ 0 & \frac{\alpha+\gamma}{2} & \frac{\alpha-\gamma}{2} \\ 0 & \frac{\alpha-\gamma}{2} & \frac{\alpha+\gamma}{2} \end{pmatrix}$$

$$\mathbf{U}_6 = \begin{pmatrix} \beta & 0 & 0 \\ 0 & \frac{\alpha+\gamma}{2} & \frac{\gamma-\alpha}{2} \\ 0 & \frac{\gamma-\alpha}{2} & \frac{\alpha+\gamma}{2} \end{pmatrix}$$

Cu<sub>69</sub>

Al<sub>27.5</sub>

Ni<sub>3.5</sub>

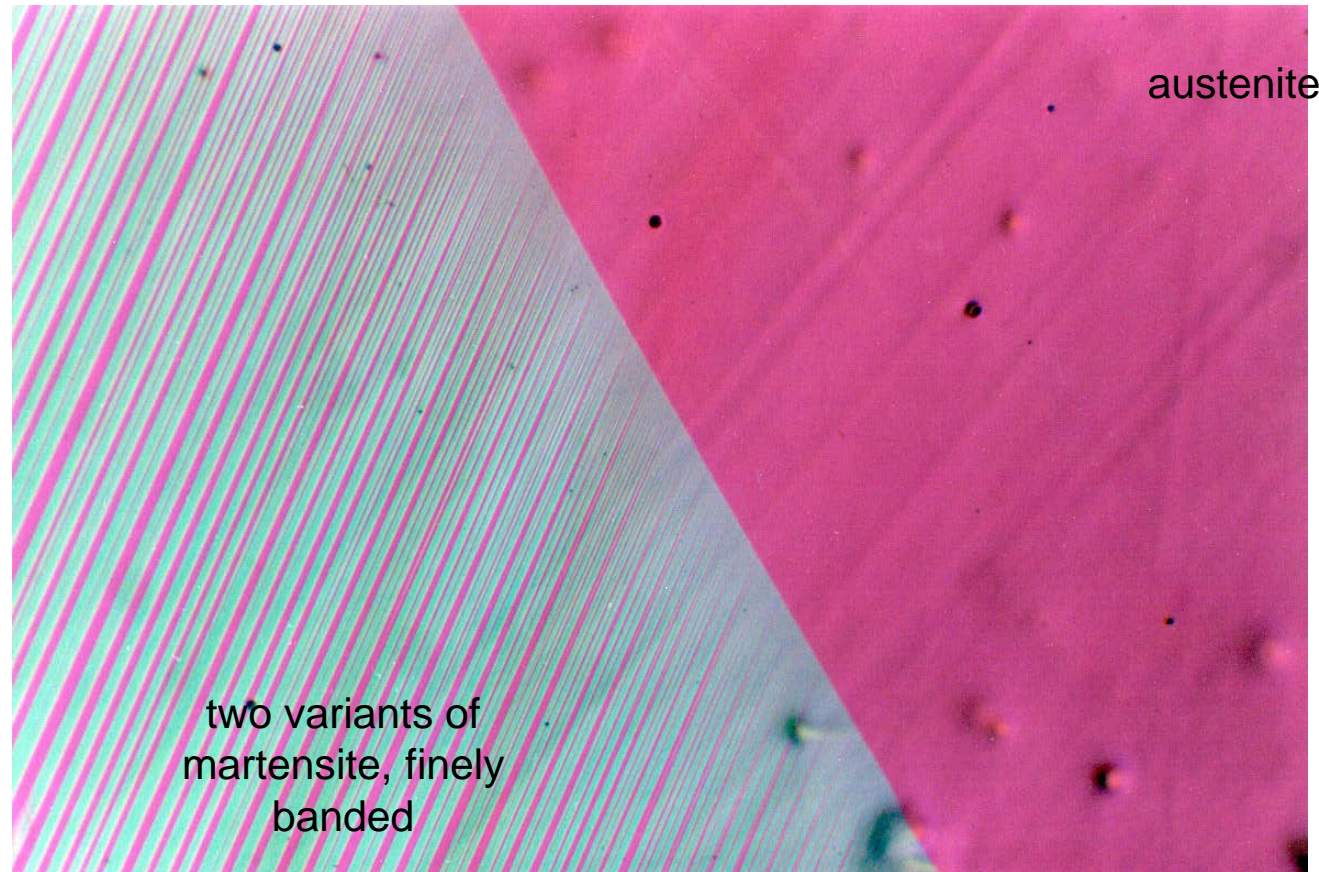
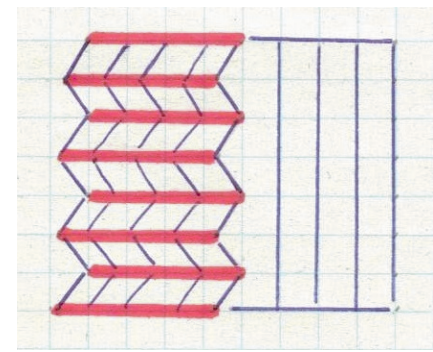
$\alpha = 1.0619$

$\beta = 0.9178$

$\gamma = 1.0230$

# The austenite/martensite interface

The typical mode of transformation when  $\lambda_2 \neq 1$



10  $\mu\text{m}$



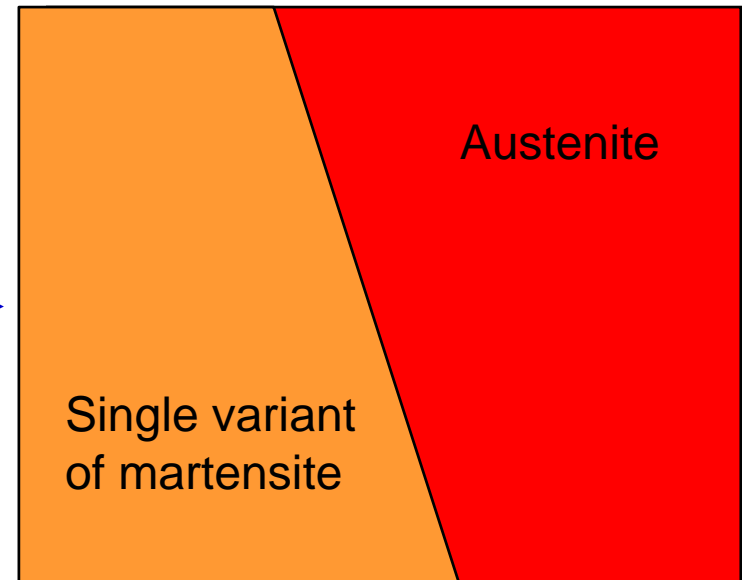
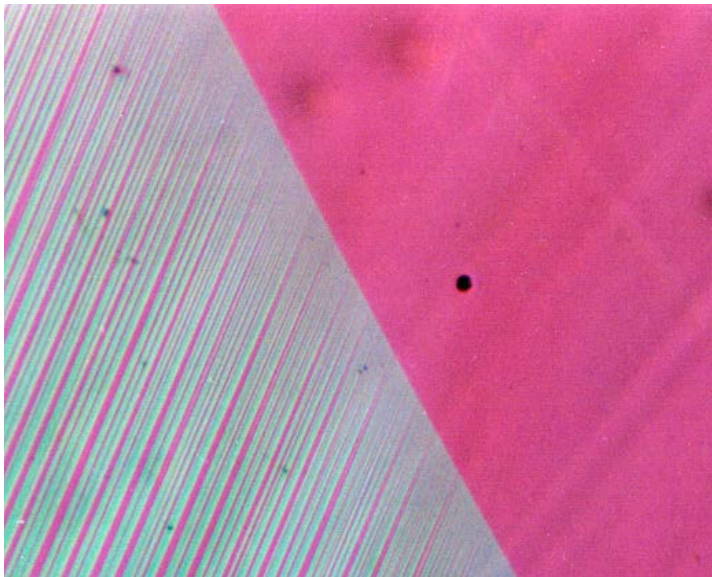
# A suggestion from mathematics

The lattice parameters  $\alpha, \beta, \gamma$  depend on composition

Can we tune the composition of the material so that a single variant of martensite is compatible with austenite?

$$\mathbf{U}_1 \stackrel{\text{for example}}{=} \begin{pmatrix} \frac{\alpha+\gamma}{2} & \frac{\alpha-\gamma}{2} & 0 \\ \frac{\alpha-\gamma}{2} & \frac{\alpha+\gamma}{2} & 0 \\ 0 & 0 & \beta \end{pmatrix}$$

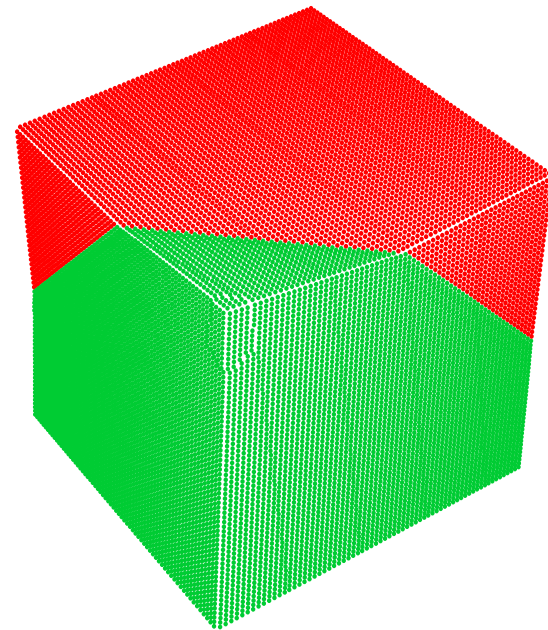
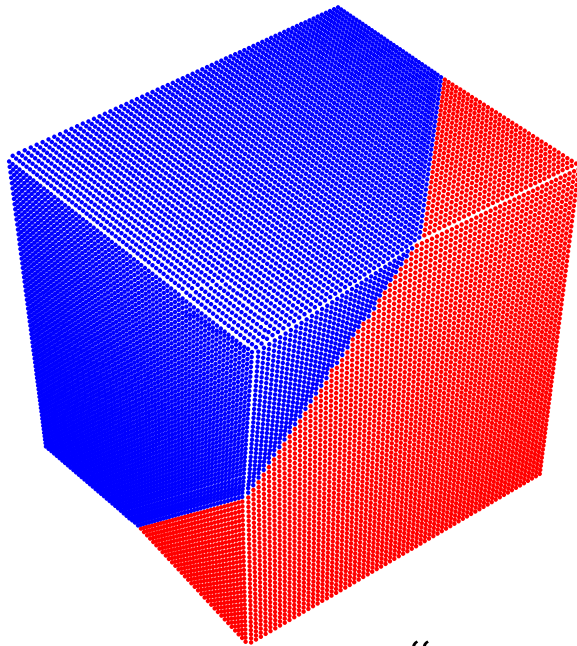
eigenvalues  $\lambda_1 \leq \lambda_2 \leq \lambda_3$



**Lemma**  $\lambda_2 = 1$  is necessary and sufficient that there is  $\mathbf{R} \in \text{SO}(3)$  such that  $\mathbf{R}\mathbf{U}_1 - \mathbf{I} = \mathbf{a} \otimes \mathbf{n}$ .

$$\text{for example } \mathbf{U}_1 = \begin{pmatrix} \frac{\alpha+\gamma}{2} & \frac{\alpha-\gamma}{2} & 0 \\ \frac{\alpha-\gamma}{2} & \frac{\alpha+\gamma}{2} & 0 \\ 0 & 0 & \beta \end{pmatrix}$$

eigenvalues  $\lambda_1 \leq \lambda_2 \leq \lambda_3$

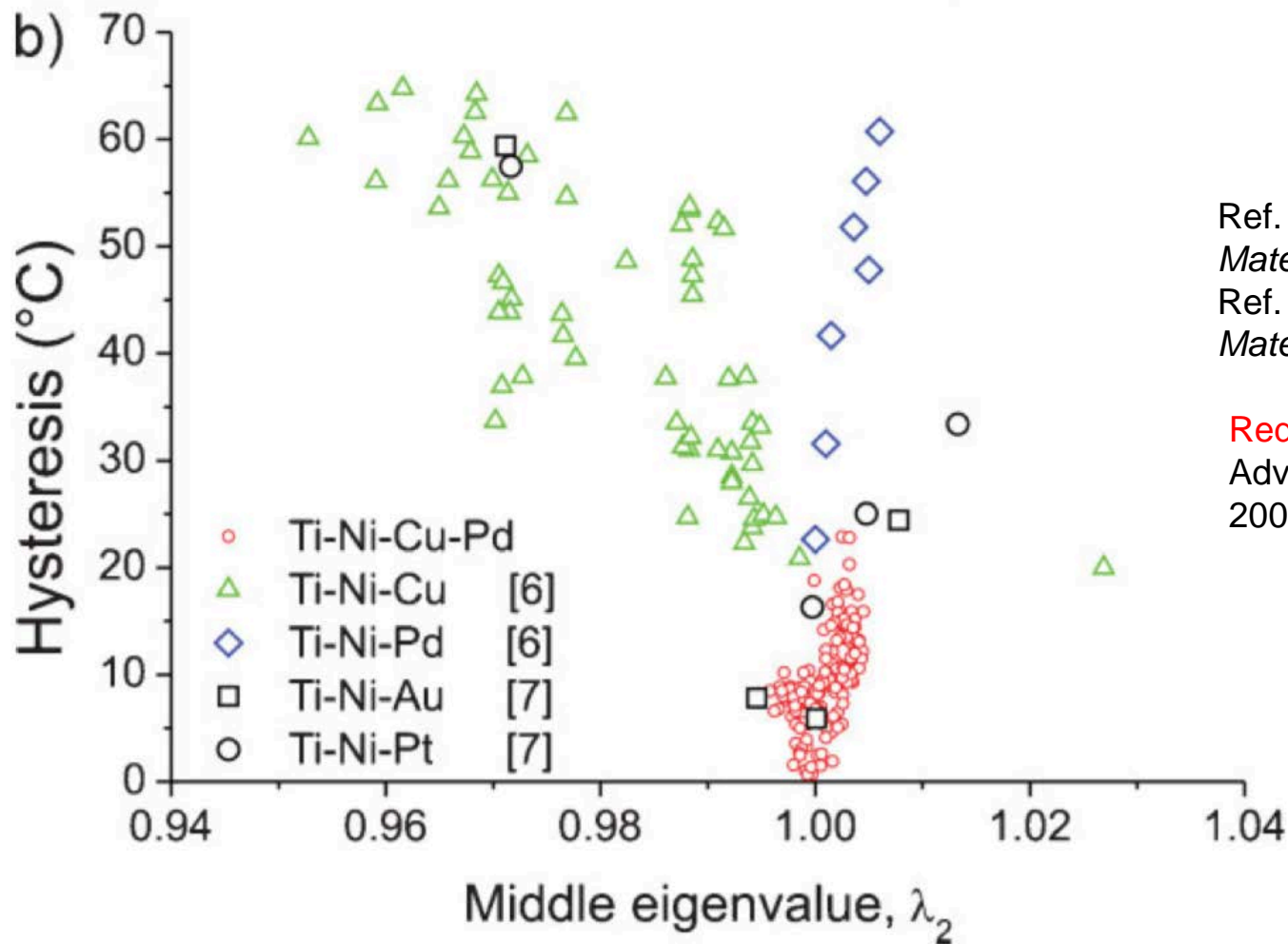


“supercompatibility”

Complete removal of stressed transition layers between phases



# Hysteresis vs $\lambda_2$



Ref. 6 J. Cui et al. *Nature Materials*, **5**, 286 (2006),  
Ref. 7 Z. Zhang et al., *Acta Materialia* (2009)

Red: Zarnetta et al.,  
Adv. Funct. Matls,  
2009

# The cofactor conditions

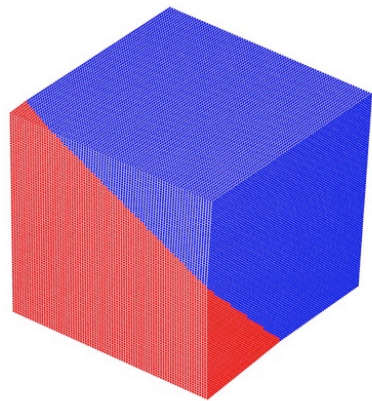
cofactor conditions

$$\lambda_2 = 1$$

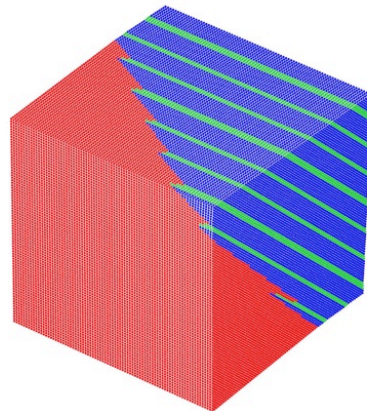
$$\mathbf{a} \cdot \mathbf{U}_1 \text{cof}(\mathbf{U}_1^2 - \mathbf{I})\mathbf{n} = 0$$

$$\text{tr} \mathbf{U}_1^2 - \det \mathbf{U}_1^2 - \frac{1}{4}|\mathbf{a}|^2|\mathbf{n}|^2 - 2 \geq 0$$

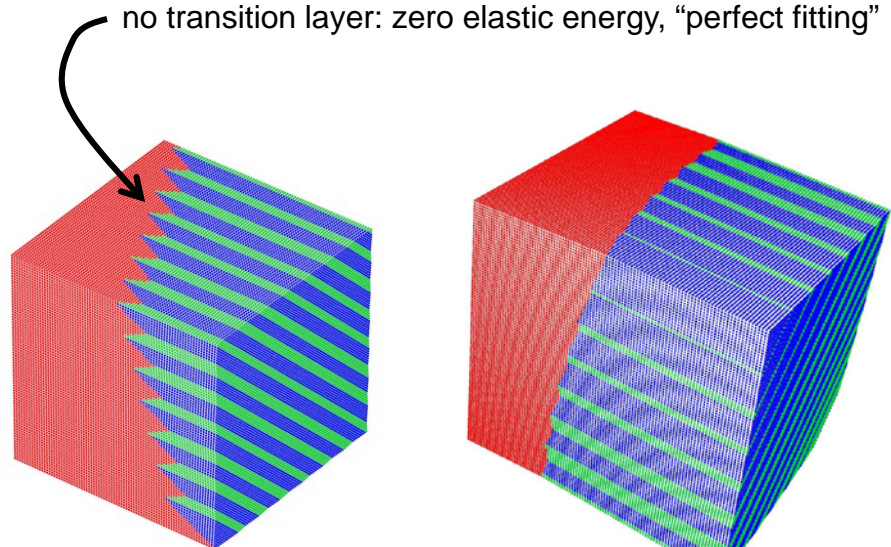
Example: Type I twins



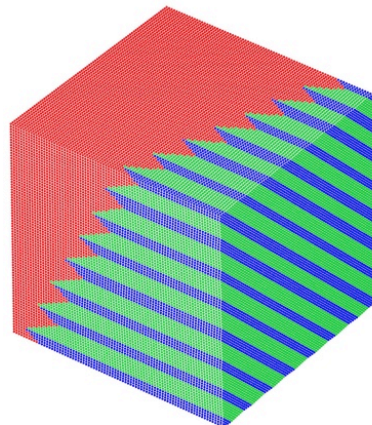
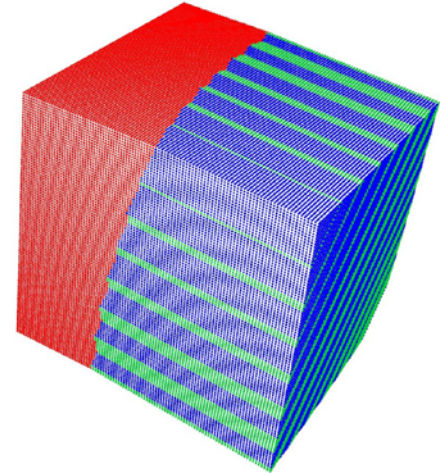
$f = 0$



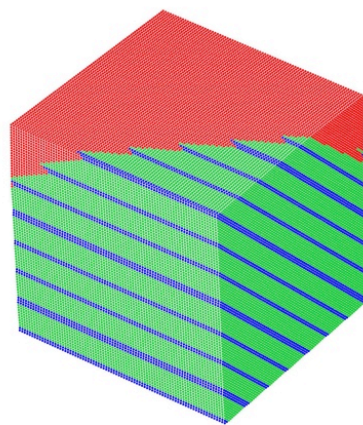
$f = 0.2$



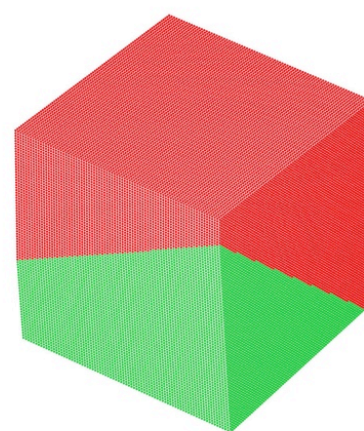
$f = 0.4$



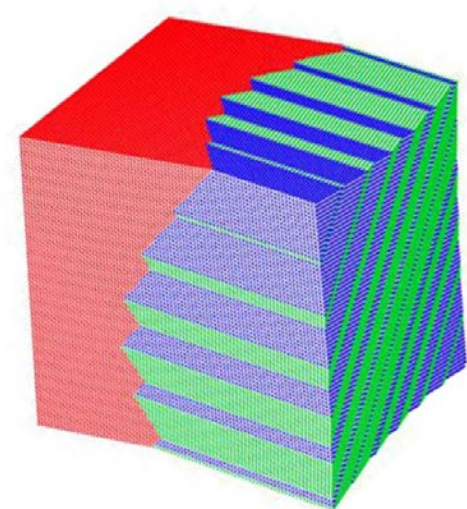
$f = 0.6$



$f = 0.8$

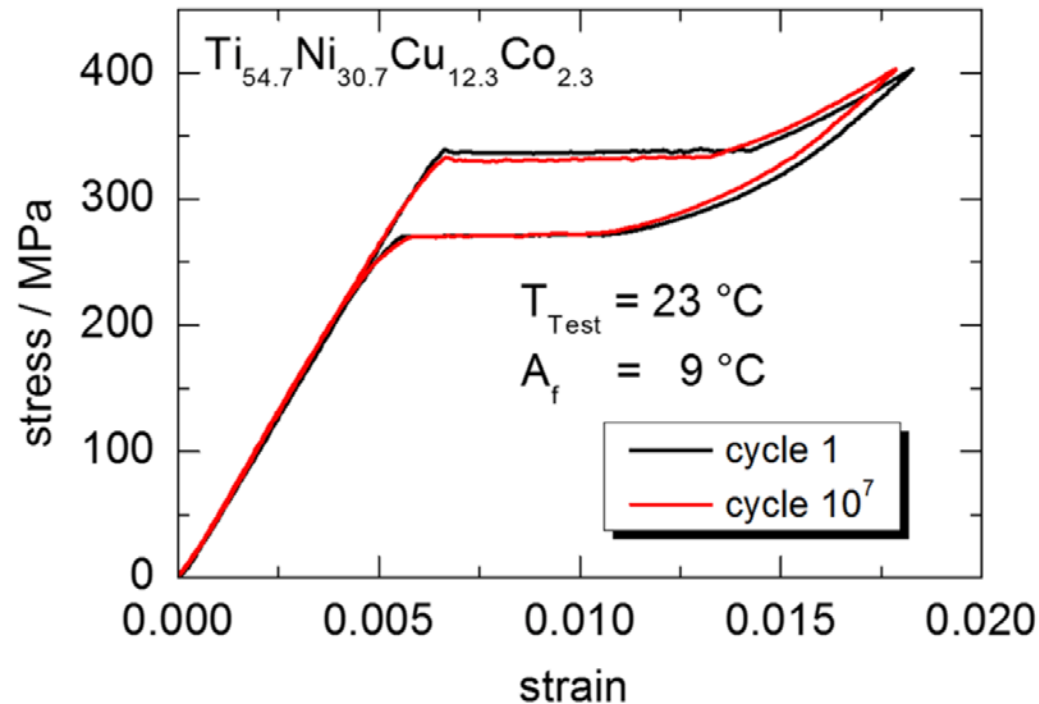


$f = 1$



# Alloy satisfying the cofactor conditions

C. Chluba et al., Science (2015) (Laboratory of Eckhard Quandt, University of Kiel)



Currently, there is a worldwide search for new supercompatible alloys



# What other mathematical challenges lie nearby?

Today's discussion has focused on shape-memory materials, but there are many cross-cutting issues. Here are two:

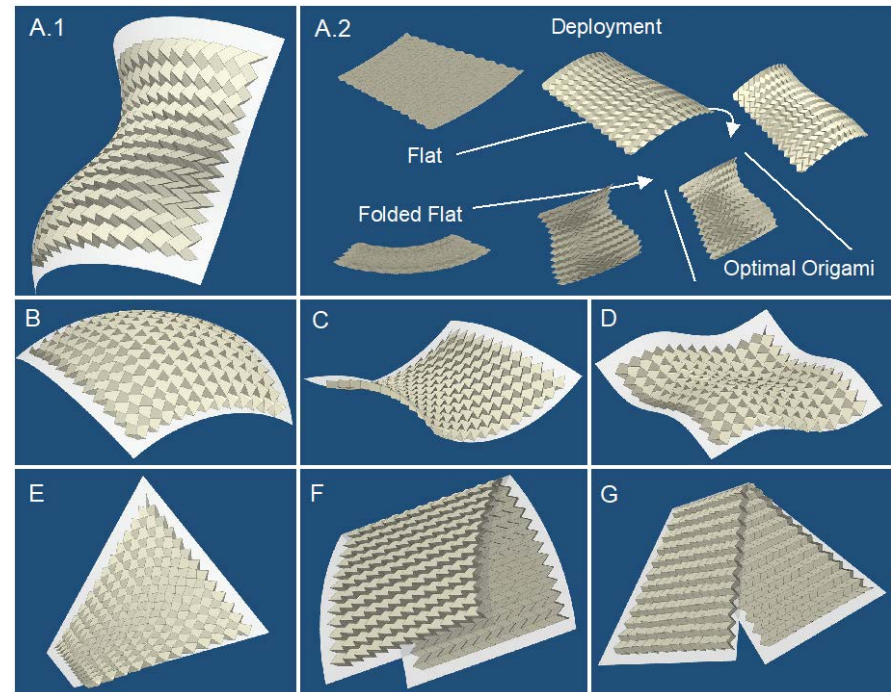
## (1) The deformations possible in a system depend sensitively on its structure

Another example of current interest: **deployable origami** (architectural design, therapeutics, deployable space structures, medical stent design, antenna design, robotics).

Goal: prescribe fold lines on a flat sheet so that

- It has a one-parameter family of (partially) folded configurations, and
- this family passes through a good approximation to a specified surface

See recent work of X. Dang et al, arXiv:2008.02349.

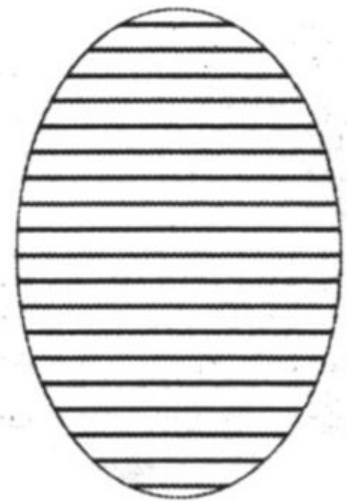


# What other mathematical challenges lie nearby?

## (2) Patterns and microstructure arising in other variational problems

### Geometry-driven wrinkling

- In recent experiments, regions cut from a thin spherical shell were flattened by floating on water (Albarrán et al, arXiv:1806.03718)
- The wrinkling patterns are robust, and they depend on the region's shape
- Recent work by Ian Tobasco explains these patterns (arXiv:1906.02153).





# Conclusions

- Shape-memory materials are useful because they sustain large deformation with little damage
- Mathematical understanding of the mechanism revealed that certain non-generic alloys avoid the need for microstructure, leading to less damage and improved behavior
- The theory involves calculus of variations problems with multiwell energies
- This is but one of many areas where the calculus of variations interacts with mechanics, in ways that challenge and enrich both fields

# ILLUSTRATING MATHEMATICS

## Supercompatibility and the Design of Materials

Please submit questions using the Q&A button in the zoom menu.



**Richard James,**  
University of Minnesota



**Robert Kohn,**  
New York University



**Irene Fonseca,**  
Carnegie Mellon University  
(moderator)

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